

Solar orbiter

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Design & layout of EUS for Solar Orbiter.

Summary.

- Requirements: Spatial, spectral, collecting power.

- Telescope options:
 - Front-end grating + 1-mirror telescope (Univ. Padova)
 - 2-mirror on-axis (strawman).
 - 2-mirror off-axis.

- Instrument layout.
- Spectrometer with holographic grating.
- Basic tolerances.

Imaging.

Spatial: 0.5arcsec pixel, FOV 34 arcmin. } Square detector
Spectral: 580-630ang, in 34 arcmin } ~ 4000 x 4000

Collecting power.

$4 \cdot 10^{12}$ photons/cm².sr per second (typical line)

$\lambda \sim 600$ ang

$t \sim 1$ second exposure

Spatial.

APS detector, min. size $p \sim 5\mu\text{m}$ for min. focal length FL

$$\text{FL} = p / (0.5 \text{ arcsec}) = 2.06 \text{ metres}$$

$$\text{Detector size } 4000 * 5\mu\text{m} = 20\text{mm}$$

Spectral.

$$\sin \beta - \sin \alpha = m \frac{\lambda}{d}$$

$\beta = 0$ - normal incidence at detector $m = -1$

1st-order differential with respect to λ :-

$$\Delta \beta \approx - \frac{\Delta \lambda}{d}$$

$$\frac{20\text{mm}}{R} \approx \frac{50 \text{ Angstrom}}{(1/4800 \text{ gr/mm})}$$

(1:1 imaging,
conservative grating technology)

$$R \sim 800\text{mm}$$

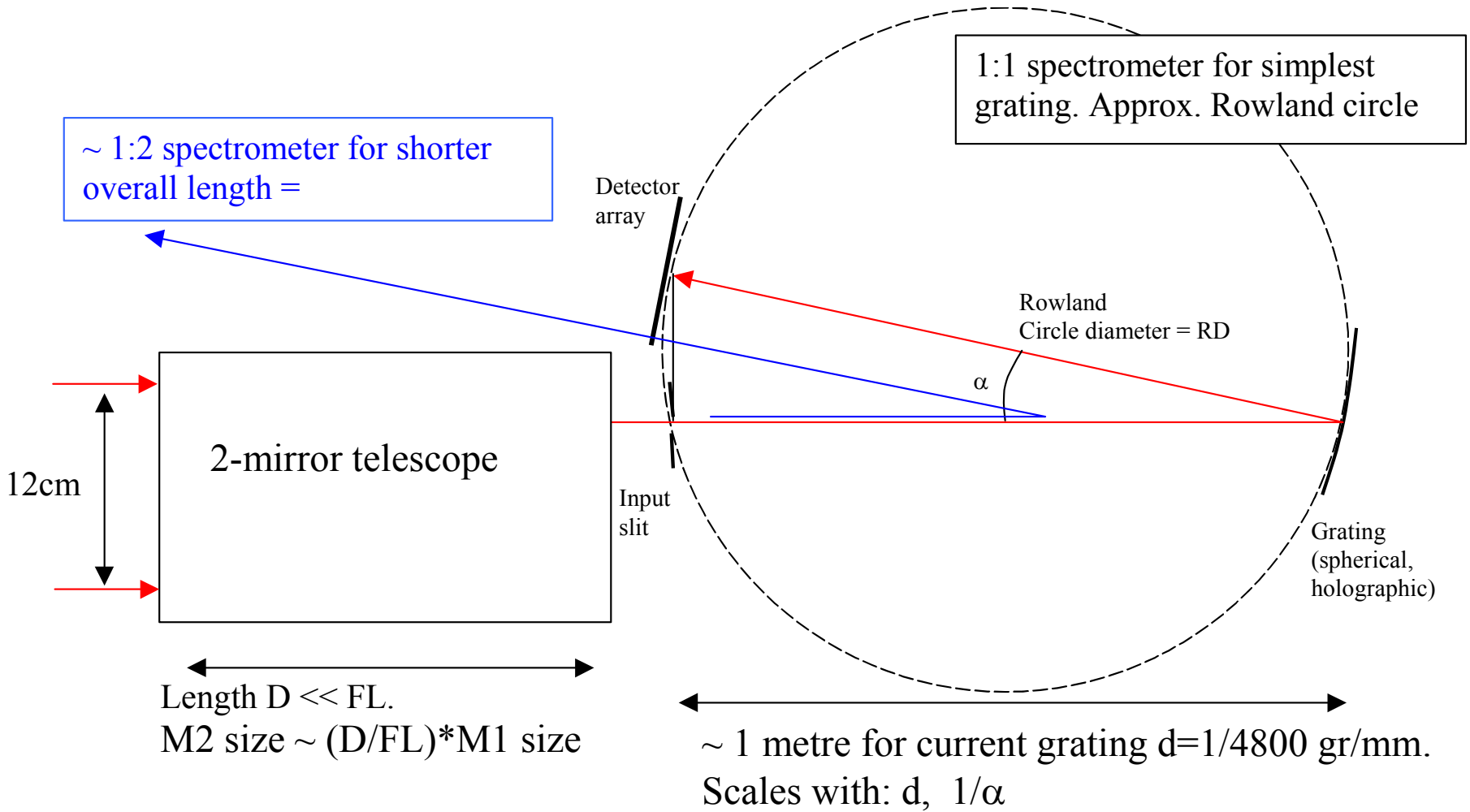
Parameter	Name	Value	Units	Comment
eta	detector efficiency	0.4		
tau	mirrors throughput	0.008		3 mirrors
g	grating efficiency	0.3		
B	photon radiance	4.00E+12	photons/cm ² .sr	
A	aperture area	113.097336	cm ²	12cm aperture
omega	pixel fov solid angle	5.8758E-12	steradian	0.5 arcsec pixel
t	exposure time	1	seconds	
Product		2.55	photons	

- 12cm aperture is reasonable limit given heat load problem

$$\implies F\text{-number} = 2.06/0.12 \sim 17$$

$$\text{Solar: } 1371 \text{ watts/m}^2 * 25 * 0.0113 = 390 \text{ watts.}$$

- Have to limit to 3 reflections.



1. Front-end GI grating + single mirror telescope + spectrometer.

- Previously proposed (Univ. Padova) to separate heat at front-end.
 - Light is pre-dispersed before spectrometer input slit.
- Relatively large size $\sim 2\text{m} \times 0.2\text{m}$, tilted.
- Single mirror telescope (parabola), aberration control only at limited FOV
 - Spatial: Possibility to improve via grating design.
 - Spectral: No improvement possible after entrance slit.
 - Assume 1m focal length (requiring 1:2 spectrometer), have $\sim 15\mu\text{m}$ spot size at slit at FOV edge.

2. Good aberration control over required FOV.

• Image (slit) plane close to M1 to minimise length.

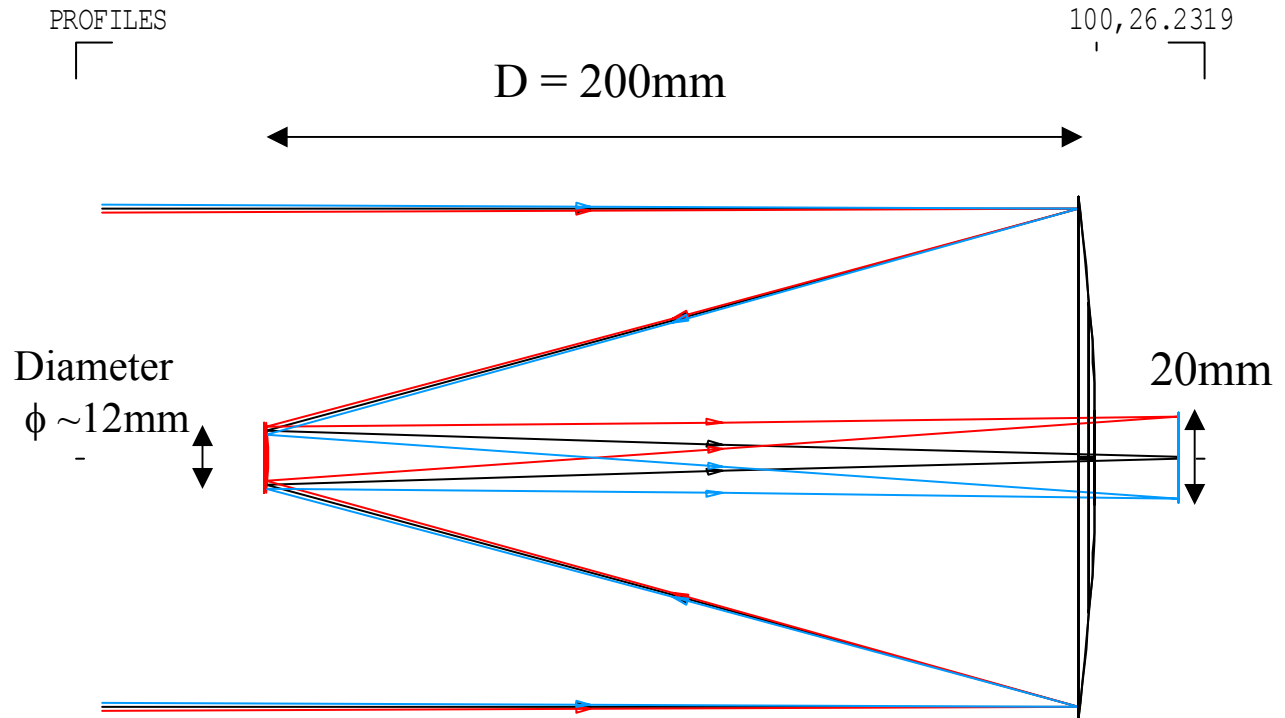
• $\phi_{M2} \sim (D/FL) \cdot \phi_{M1}$

• $D \sim 200$ to 400 mm

$(D/FL) \sim 10$ to 20 %

$\phi_{M2} \sim 12$ to 24 mm

• Well-corrected, but
Field curvature ~ 2 mm



Heat dissipation.

Load on M2 is high, due to :

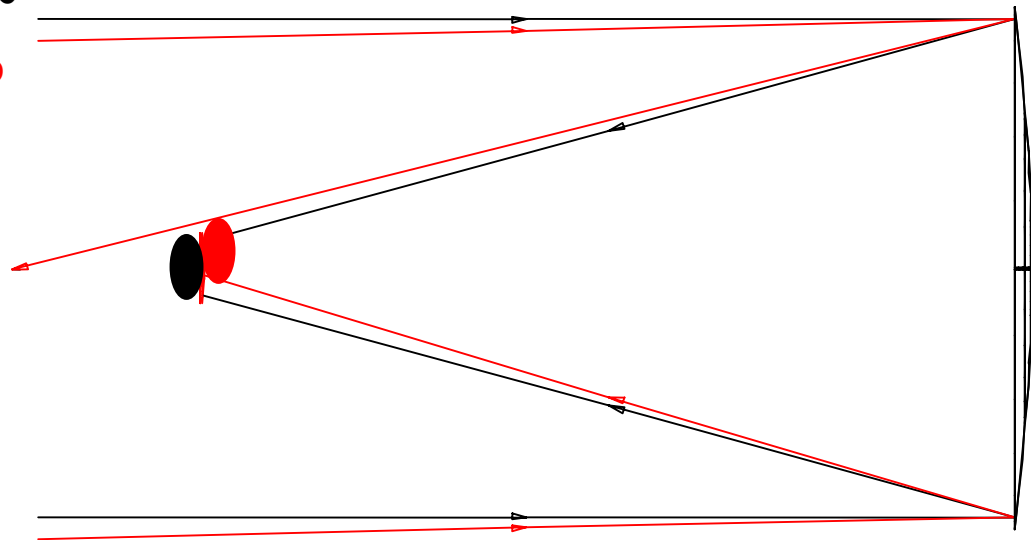
Beam concentration.

Limited motion of beam on M2 versus field angle :-

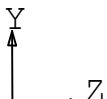
100,26,2319

Sun centre

Sun limb



- ~ 80% of power from M1 hits M2
- M1 must be thermally absorbing
- Stringent opto-mechanical design
- large radiator panel needed

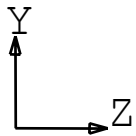
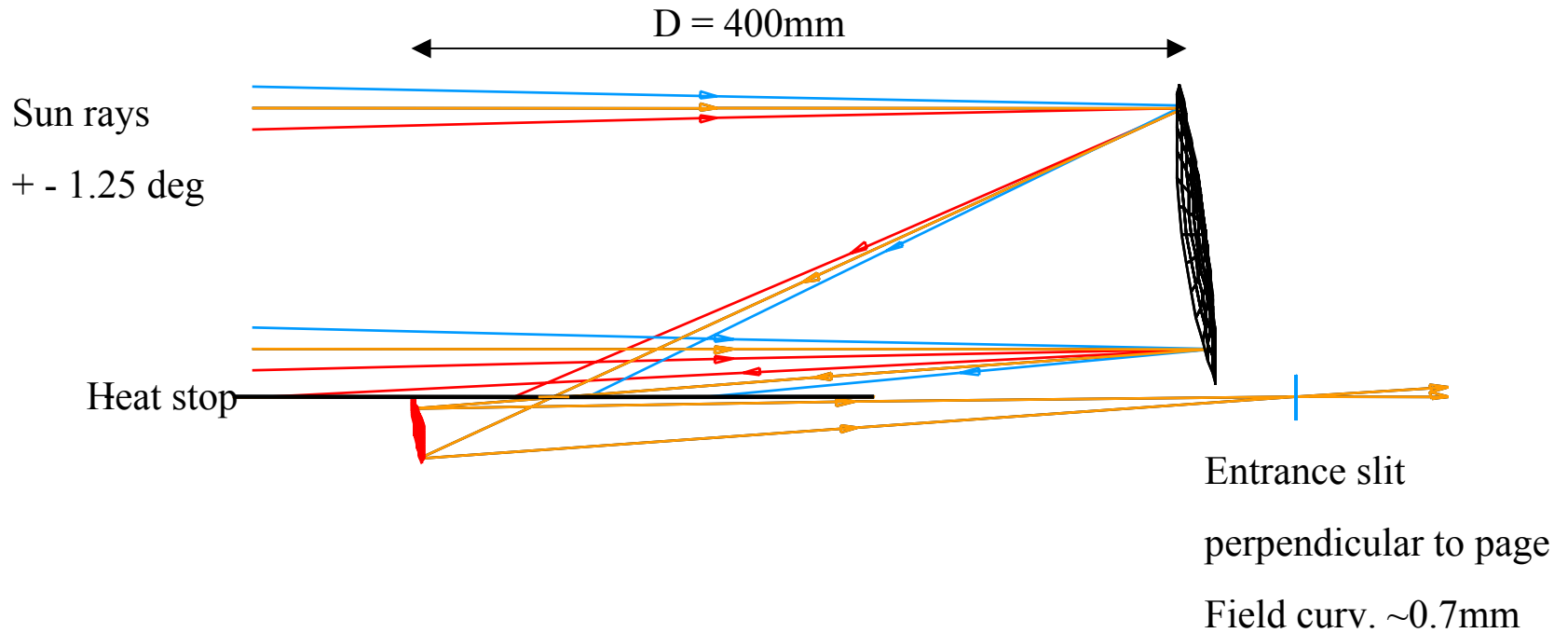


PROFILES

307.017, 115.962



Off-axis telescope & rays from full solar disc, blocked at heat stop



-184.294, -553.362 mm

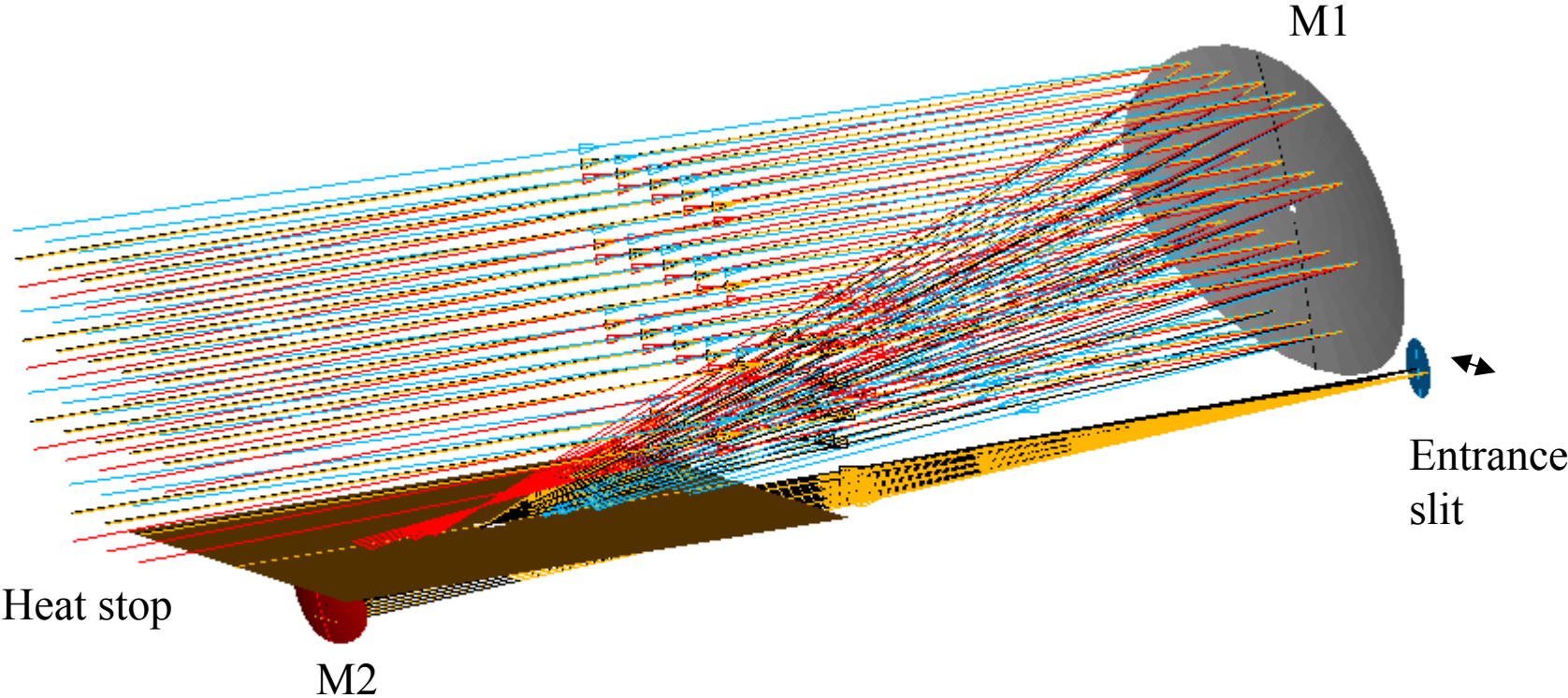


ASAP Pro v7.0

2001-11-27

13:51

- Solar image in M1, size $\sim 2.5\text{deg} \times 400\text{mm} = 17\text{mm}$
- Heat stop aperture has to be curved & oversized due to aberrations.
 - select e.g. $34 \times 10 \text{ arcmin} = 2\%$ of solar power
 - Reduced flux on M2.
 - Reduced total load on spectrometer slit (same local flux)
- Design should allow M1 & stop to be heat-reflecting.
 - Reduced total absorbed power & so relaxed the cooler & radiator requirements.

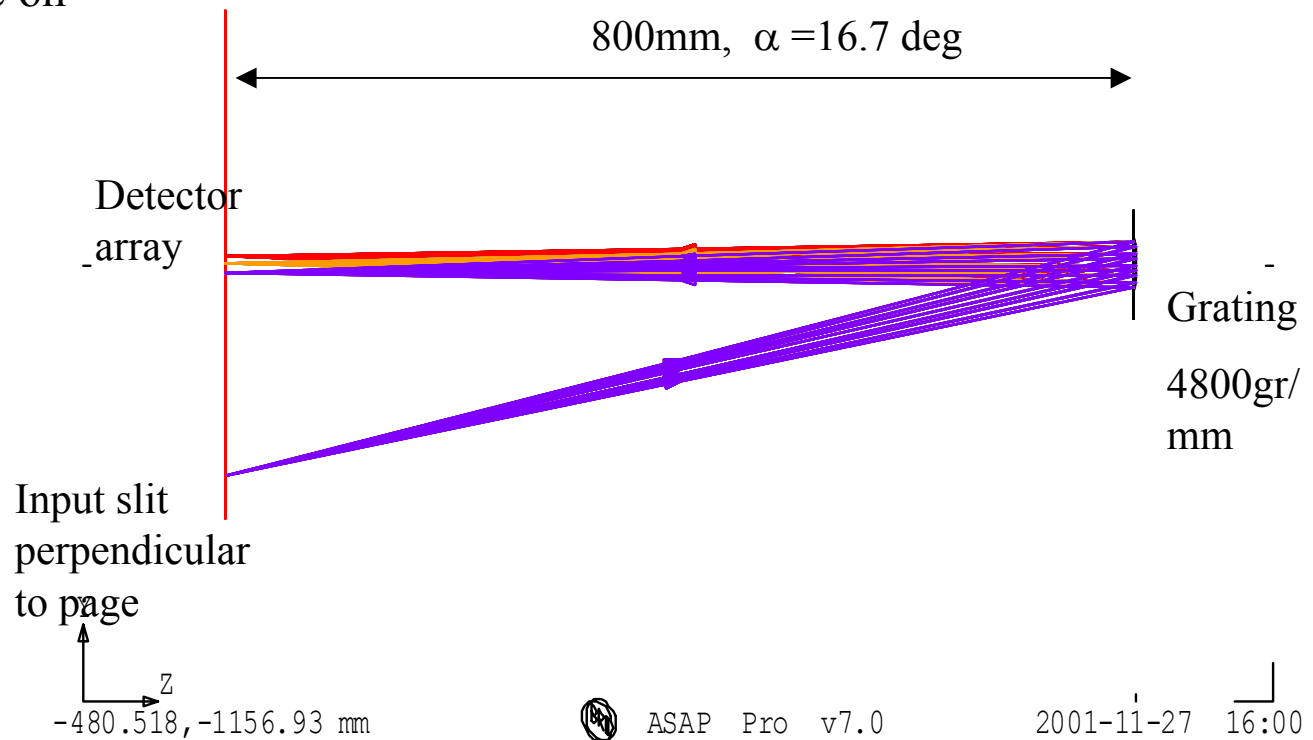


1:1 design, spherical variable-space holographic grating.

1:1 spherical VLS grating

480.519, 152.301

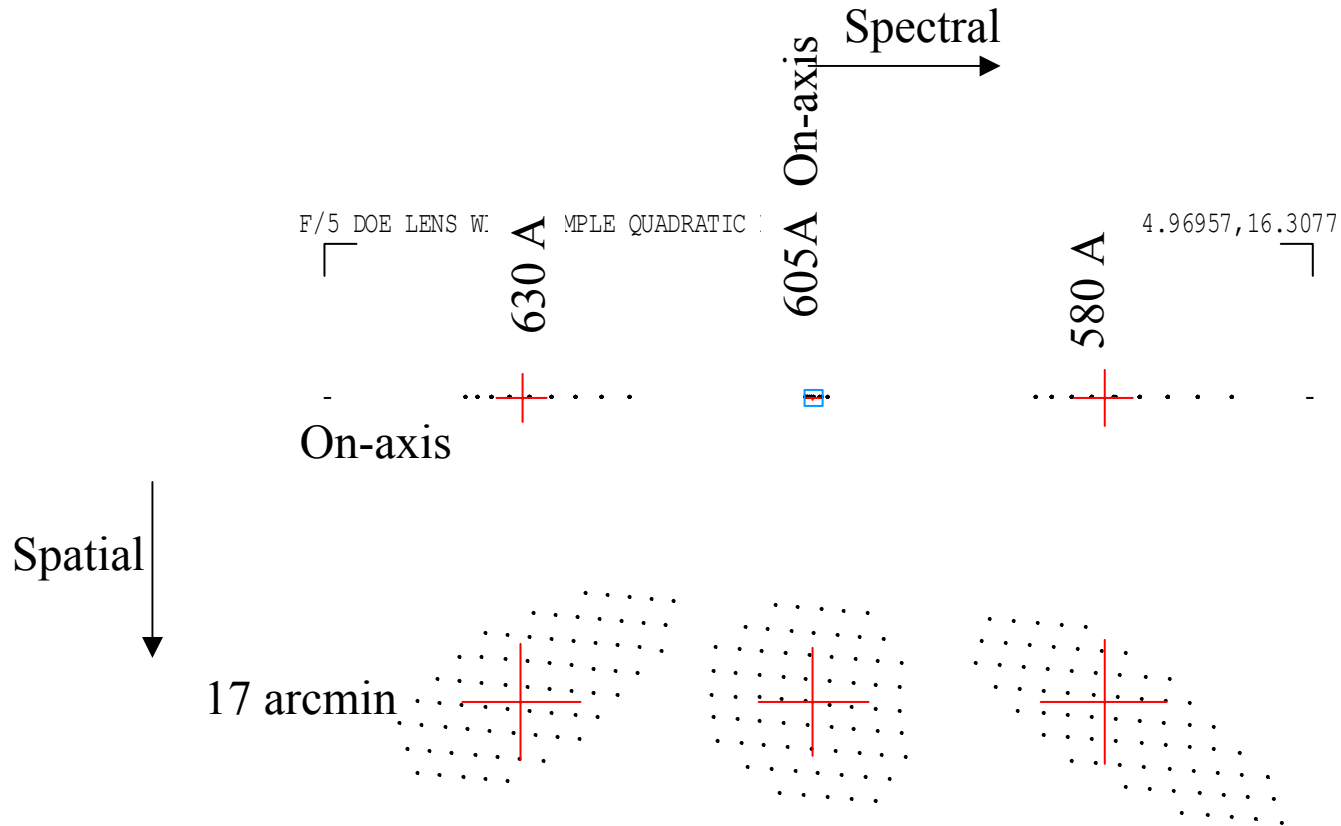
- Normal incidence on detector.
- Off-rowland for holographic form
- 580-630 Angst



1:1 design, spherical holographic grating.

Spot diagram cf. 10um square (shown in blue)

Hologram provides insufficient correction, need higher order grating function.



1. **absolute wavelength** calibration, i.e. No requirement for stability between ground & use. The spectrometer is self-calibrating in flight by being able to recognise known spectra.

2. **Pointing** is also calibrated in flight, e.g. by position of the solar limb.

(If these calibrations weren't so, optics would have to be stable to < 1 pixel, 0.5arcsec.)

3. **Telescope Focus**. If the focused spot were allowed to degrade by 2 μm in diameter ($\sim 1/2$ pixel) at the slit, the allowable two-mirror axial separation change would be $\sim 3\mu\text{m}$, i.e. $\sim 3\mu\text{m}/200\text{mm} = 15$ ppm relative. Active focus required ?

4. **Slit axial position** to telescope. 2 μm as above multiplied by F-no =17, giving $\sim 34\mu\text{m}$.

4. **Spectrometer focus**. Grating axial (z) position relative to the telescope. For a 2 μm increase in spot size at the detector this motion is allowed to be $\sim 50\mu\text{m}$. Similar motions are allowed in slit & detector position WRT the spectrometer.